

A Specialized Hardware Based Design for Earthquake Warning Design and Identification of the Sensing Area Module in Remote Areas: A Practical Approach

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Abstract: *The main aim of the proposed study is to design a cost effective earthquake warning sensor based on time critical electronic control module designed by using proposed hardware components in Multisim. The proposed work consists of three parts: introducing a radon sensor unit based on volumetric analysis of radon as an earthquake precursor that acquires data count over a period of 100 days and placing the upper level of the sensor in water. When the water level tilts, the hardware device immediately activates the circuit designed in Multisim. The circuit design uses readily available electronic components including a LM324N op-amp and a NE-555 timer circuit able to detect electrical and environmental characteristics and is capable to analyze low frequency components that are equivalent to movements incorporated as a result of this tilt to respond with the alarm. We present the general architecture of the circuit and design of the circuit concerned with the circuit description and operation, design flow chart and implementation of the sensor. Thirdly, we create boolean sensing range for a radon detection unit and analyze how an inner and outer circle can identify the 'Earthquake Preparation Zone' or the seismogenic zone corresponding to an earthquake occurrence.*

Keywords: *Sensor, Electronic Control Module, Earthquake Warning, Radon Monitoring Unit*

1. INTRODUCTION

Despite all the scientific advances in the field of earthquake prediction, the idea of accurate prediction and monitoring of earthquakes still remains a vision of the future. Although many techniques have been implemented and the avenues of scientific warning based on interdisciplinary analysis of electronic instrumentation, geophysical explanation and a consistent time margin between a potential warning and its eventuality remains a dream for scientists around the world; there is also a need to simultaneously get rid of any possibility of erroneous detections leading to false alarms associated with the different earthquake patterns and associated stress-strain interactions between the geophysical parameters and precursors. In order to extend the scope of analysis of the temporal and spatial evolution of stress in the different stages of the fault system associated with the complexity of the fault geometry, heterogeneity, and anisotropy of the rock for the host rock media exhibiting highly variable behavior in the incipient region (Schulz et al., 1973; Srivastava, 1983) so that a plausible earthquake early warning system can be developed for earthquake risk mitigation for the region. There are three basic reasons we feel that earthquake prediction analysis has suffered due to the absence of reliable diagnostic precursors for different geo-tectonic settings responsible for earthquake genesis. Existing Earthquake Warning Systems (EWS) are often based on a deterministic approach which led to many false alarms after the strong faulting segments accumulate strain to become areas of instability (Dutta et al., 2012 a,b). Secondly, sudden occurrence of earthquakes and their incipient source showing precursory behavioral patterns (Dutta et al., 2013a) occurring in different parts of the world were associated with smaller response time that pre-detect a certain cluster of earthquake patterns (Dutta et al., 2012c). Thirdly, adoption of available earthquake resistant building codes assimilated up to a particular size of earthquake by several earthquake prone countries is also not apt to ensure reduced degree of earthquake hazards to infrastructures and vital structures located in seismically active regions. These constraints are prevailed because the process of earthquake genesis is found to be dynamic and the generating mechanism remains completely uncertain in terms of size and its depth of occurrence (Mishra, 2007). *Figure 1* shows the structural frame of the electronic detection device with its operating principles. Passive seismological

parameters identified using GPS sensors and strain meters associated are found to occur at very low frequencies explicitly identified as a data count. It becomes increasingly difficult to maintain an inertial reference, and for the observation of low-order free oscillations of the Earth, tidal motions, and quasi-static deformations as strainmeters may outperform inertial seismometers. Strainmeters are conceptually simpler than inertial seismometers although their technical realization and installation may be more difficult. It is thus a necessity to design a conceptual hardware module that can sense and detect over a period of time, the passive components like tilt or strain on the surface using volumetric analysis of precursory parameters generated during a continuous tectonic movement and provide onsite alarm system.

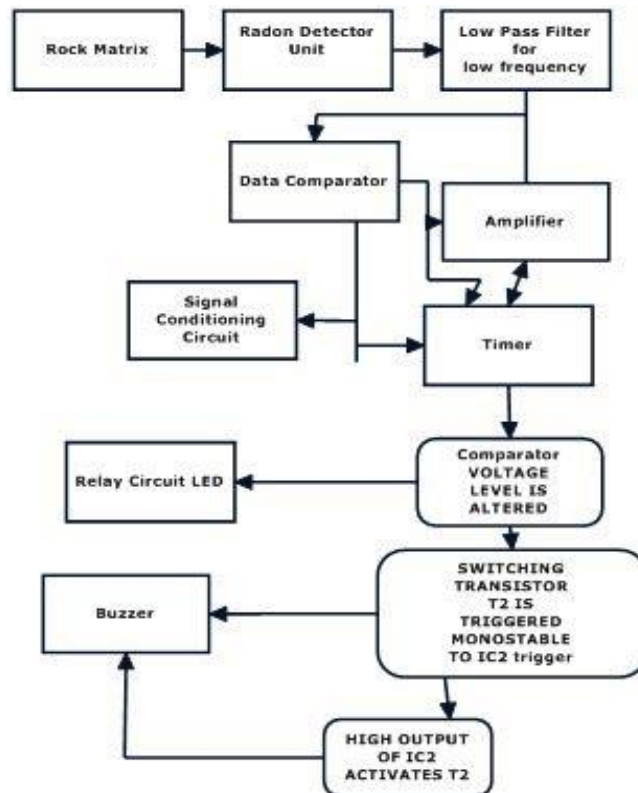


Figure1. Structural Frame of the Electronic Device Developed

The aim of this electronic device is to acquire data in the form of tilt and radon count and acts like a passive method of detection. The electronic device is aimed at sensing and detecting the change of the level of water absorbed in a Radon detection unit. The instrument designed has been developed based on the concept that the geological rock medium is a collection of arrays of rock matrix undergoing stress-related deformation at different depths. The difference of conditions of measurements of soil radon in these cases results in some data registration in the form of radon count in Volumetric Analysis of Radon (VAR). First, at such mode of selection of soil gas we deal not with true value VAR in the given point of measurement, but with some quasi stationary values VAR which is defined(determined) as properties of the system and in parameters of a data-acquisition equipment.

Second, quasi-stationary level VAR is formed as for the account emanation of radon in seized pumping volume of rocks (depression volume), and diffusion flow of radon of a file outside depression zones. At constant parameters of environment and hardware conditions of registration level of VAR the diffusive flow is found to be stable enough and constant (Outkin et al., 2006). The radon detector unit locates the position of extension and compression zones within the rock mass based on study conducted by (Outkin et al., 2013). The tectonic movements can be interpreted by resetting elastic energy leads to earthquake after reducing signal line friction and elastic strain relief (Outkin,2000) lithospheric blocks and are able to continue their movement in the original quasychaotic direction. Furthermore, a monitoring of soil radon in an active seismic region elucidated the VAR behavior reflecting compression and extensional stress during rock mass surface bending in connection with geodynamic processes. Based on the experiments, a new model is proposed here for the precursors to geodynamic events and their connection with radon exhalation.Radon is an inert gas

that is produced by the radioactive decay of uranium and other elements in rocks. Because Radon is inert, it does not combine with other elements to form compounds, and thus remains in a crystal structure until some event forces it out. Deformation resulting from strain may force the Radon out and lead to emissions of Radon that show up in well water. The newly formed micro-cracks discussed above could serve as pathways for the Radon to escape into groundwater. Preparation and realization of the tectonic events are studied on the basis of analysis of monitoring data of radon (radon activity 3-d VAR) (Chu-Yu-King, 1991; Outkin et al., 2006). Content of radon in the air about 10^{-16} %), so it may not, in principle, affect the behavior of the mountain massif under compression-tension, but radon is soil air and can serve as a good indicator of changes in consistency of the air and the pressure of the gaseous phase.

2. OVERVIEW

The lithospheric blocks remain almost without fracture, but is substantially changed configuration (location) units and the interblock structure. When further movement of blocks may repeat the described situation and occurrence of earthquakes in another part of the seismogenetic area. This model is verified by radon monitoring (Chu-Yu-King, 1991, Outkin et al., 2006) and allows tangible ways of prediction of tectonic earthquakes. In this study, a radon detector unit proposed by Outkin et al. (2012) shows a convective phenomenon is found to take place as the water flows along the borehole in response to the hydraulic gradient that occurs due to stress induced earthquake. It was used for compulsory pumping soil gas from the air-tight sealed chink by depth of 2-3 m.

2.1. Sensor Model for Measurement

The instrument is based on experience gained technique of measurements with forced hole degassing developed by (Kozlova and Yurkov, 2005) shown in Figure 2, and has the following requirements: The instrument must determine the average value of radon concentration (RC). The processed data may be completely transferred into a PC. The sensor is based on convective technique whereby soil gas is pumped out from the tube (whereby the water head pressure in the latter decreases to 20–30 mm) and then flows to the instrument which measures radon concentration in the gas flux. In this case, radon influx into the rarefied space is from a much larger effective collection zone of a radius of ~700 mm. This modification increases the sensitivity of the measurements by a factor of three approximately and, at the same time, reduces the tidal and weather noise. The results of the measurements are stored in memory every hour, along with the time measurements. Minimum concentration: concentration determined with a statistical error equal to $\pm 20\%$: 80 Bq/m³ for 1 hour of measurement. Maximum concentration: about 150 kBq/ m³.

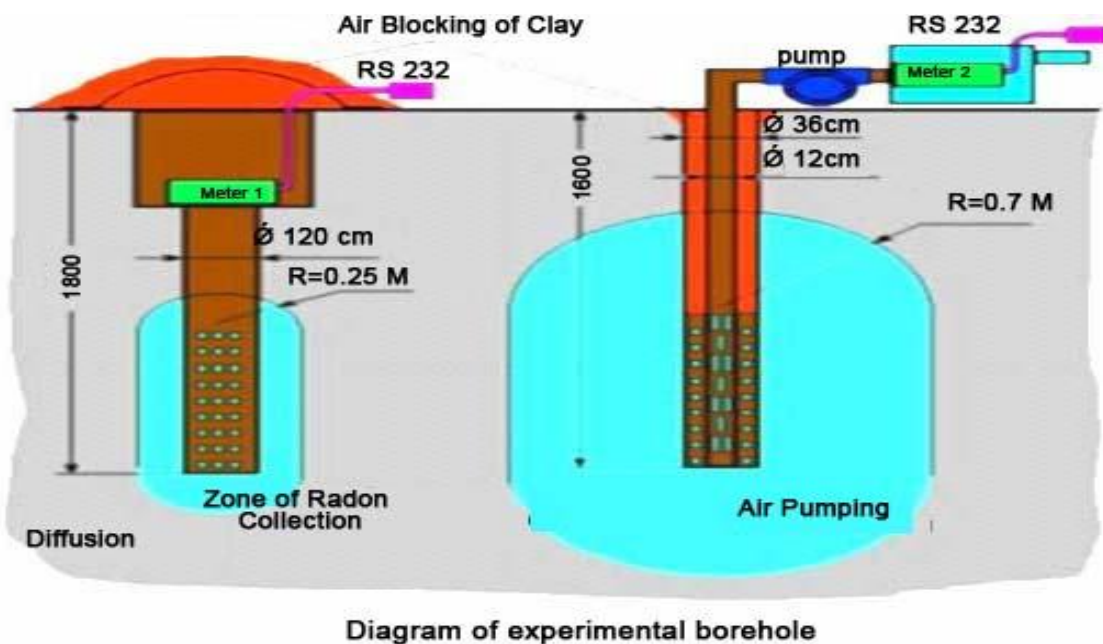


Figure 2. Diagrams of the equipment which was used in experiment on Northern Tian – Shan (Outkin and Yurkov, 2010; Outkin et al., 2012)

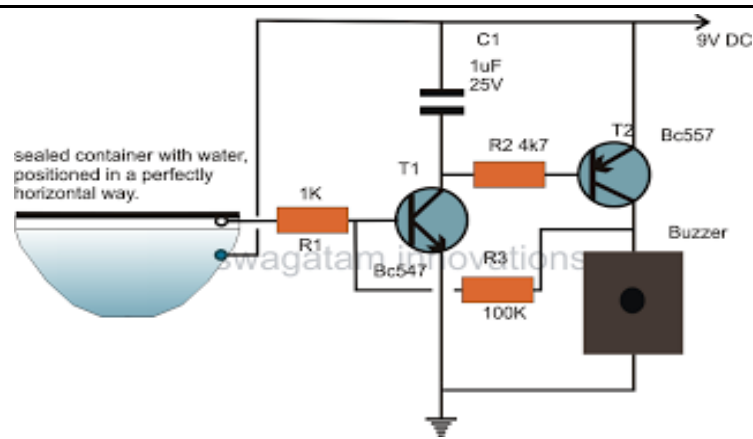


Figure3.

The data on VAR due to convective measurement technique yields more information about increase of speed of migration of radon in the rock fracture which increases approximately by 2-4 times of the normal showing an anomaly and increases three times the normal as observed for any detector of radon on depth about 3 meters (On Northern Tian-Shan VAR has increased almost up to 5000Bk/m³ instead of 1500 Bk/m³). Second, a level of daily variations due to daily tidal movements shows that 5-7 % from average size VAR (instead of 40-50 % in radon diffusion coefficient) is reduced. Thirdly, it is observed for deep bores, the detector influence of atmospheric pressure on data VAR is practically eliminated. In such a scenario, the SNR can be further improved by aggregating data from the right groups of cells that tend to experience the first shakings together (co-activated") accuracy of detection and localization (estimating the initial location) of geospatial events as a function of sensor and event parameters. It has been found that such geo-spatial events generate acoustic radiation (acoustic emission) which is registered as continuous noise variation in regions with high seismic activity and forms underground background sound. Formally, any disruption of solidity is an earthquake; the difference lies in place and the amount of the emitted energy. Special hoist (logging-hoist) is used in which measuring equipment is set and connected by digital communication channel with the central point of control according to RS-232 mode. When piezoelectric ceramics are used as sensors, there is usually some noise in the measure voltage. All sensors of radon located with merged in modern radio channel(Dutta et al., 2013b) which analyzes the data obtained for defined behavior for dilatancy sizes and approximately sensors of radon (radon special sensors) located within our region of interest merged in modern radio channel with some data processing centre, which, we assume, analyzes the data obtained, inter alia, defines behavior VAR dilatancy zone (Outkin and Yurkov, 2010), their size and approximately the expected power events, as well as the position of the epicenter.

3. CONCEPTUAL DESIGN OF WARNING AND ALERT SYSTEM

The project work presented the design and implementation of seismic sensors for industrial and domestic purpose using the radon detector unit and a buzzer with its underlining principle of piezoelectricity. The circuit uses readily available components and the design is straight forward. A standard piezo sensor is used to detect vibrations/sounds due to pressure changes. The piezo element acts as a small capacitor having a capacitance of a few nanofarads. I've overcome sensor measurement noise by an analog low-pass filter comprising of R7 and C11 and filtering out the measurement noise. Like a capacitor, it can store charge when a potential is applied to its terminals. It discharges through VR1, when it is disturbed. Piezo transducer would be solely able to sense high frequency vibrations and never a swaying action. An earthquake will never generate a shrill noise rather it produces a gentle swaying pattern, when it hits. Therefore using a piezo element is a flop idea. Of course a piezo would detect tremors only if it were used in the form of a load-cell, by integrating some kind of load, assembled for implementing an oscillating action during tremors. In the present earthquake sensor circuit, we have used radon detector unit as the detecting agent as shown in Figure 3. The mechanism works in principle in identification of change of water levels with change of the radon detection count. The multisim design of a Electronic module is shown in Figure 4. The top module has been designed by feeding pulses through an AC source that simulates the output from a radon detector counter. Like a capacitor, it can store charge when a potential is applied to its terminals. It discharges through VR1, when it is disturbed. In the circuit, IC LM324 (IC1) is wired as a differential amplifier with both its inverting and non-inverting inputs tied to the negative

rail through a resistive network comprising R1, R2 and R3. Under idle conditions (as adjusted by VR1), both the inputs receive almost equal voltages, which keeps the output low. The method for predicting seismic events includes identification electronic part consists of a couple of transistors rigged into a latch circuit. The input to this circuit is achieved from a small half round container filled with water. The positive supply from the circuit is dipped inside the water while the hot end of the input is placed in such a way that it stands just a mm above the water. The detection unit fitted with current electrodes (A, B) and potential probes (M, N) arranged in the ground and detecting electrical current and induced potentials by means of said electrodes (A, B) and said reception probes (M, N), for the calculation of pressure changes in the ground. The moment the level pressure reduces by 20-30mm, the hot end of the circuit with the positive terminal, dipped inside the water. The positive of the supply immersed in the water instantly makes contact with the HOT end of the circuit via water; the circuit gets triggered and immediately latches. The connected buzzer sounds, sending an alarm signal. The disturbance discharges the stored charge. This causes the IC1 to produce a high output. This high output is used to trigger switching transistor IC2 and the vibration or sound or movement made caused the buzzer to beep. The sound and vibration caused movements can also be detected by new and growing technology. As radon data provides the output, Q3 transistor is generally in dormant state and on detecting the water filled sensor assembly, the needles within the sensor container are subjected to a short-circuit caused by water with the availability of positive voltage at Q3's lower part triggering to get activated. Q3's activation triggers those of Q4. The next transistors stage which Q4 provides static bias for Q3 making it to be latched with the DC output that will pass through the comparator LM324N. LM324 is a low-noise JFET input op-amp with low input bias and offset current. The BIFET technology provides fast slew rates. The reference voltage of the LM324N is fixed with the help of R2. This alters the voltage level at the inputs of comparator LM324N and the output momentarily swings high as indicated by green LED1. This high output is used to trigger switching transistor Q1, which triggers mono stable IC2. Placing a low-pass RC filter at the output of the amplifier R4 C6 can help nullify the feed-through of high-frequency signals. The timing period of 555 timer is determined by R7 and C5. With the shown values, it will be around two minutes. The high output from IC2 activates Q2 and the buzzer starts beeping along with red light indication from LED2.

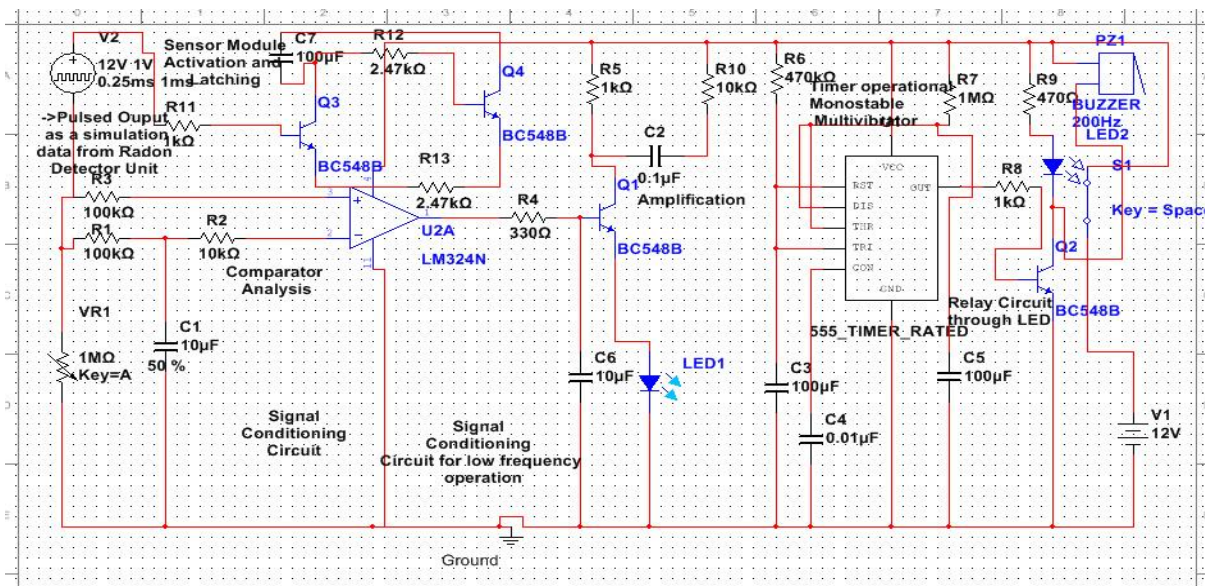


Figure4. Design of Multisim Simulation Diagram with Electronic End circuit

4. IDENTIFICATION OF THE SENSING SEISMOGENIC ZONE

The study warrants “target zone” has been defined as the study area which constituted from porous cracked saturated rocks and with high capacity of cracks growth during increasing tectonic stress. In this distinctive zone, a radon monitoring measurement in soil and groundwater has been implemented (radon precursory study in soil and groundwater is quite difference in measurement methods, but not in interpretation with seismic events). This may prove costly in earthquake warning message transmission whereby a mini delay in data transfer might collapse the entire system. The natural pre-

earthquake phenomena such as gravity variations, radon emanation, anomalous electric field and changes in meteorological parameters like temperature and relative humidity can be found statistically and empirical relation can be drawn in respect to a regression equation based on geo-spatial variables (Dutta et al., 2011). The concept of Earthquake Preparation Zone which is the first sign of an imminent earthquake is described. According to this concept all the ground based pre-earthquake signals are generated all over this zone. The size of this zone is dependent upon the size of the earthquake under preparation and may have a radius of more than 300 km for an earthquake of magnitude 6. Furthermore, use of dedicated satellites to monitor earthquake precursors from space (Dobrovolsky, 1971) has been defined for a centralized prepare zone; not for a wide area. As the target zone is a circle of radius 5 km and the monitoring station located at the center of this area, the uncertainly parameter is considered 5 km.

4.1. Earthquake Preparation Zone

The concept of earthquake preparation zone was developed by different scientists, Dobrovolsky(1971), Keilis-Borok and Kossobokov (1990) and Bowman *et al.*(1998). This is an area where the local deformations and their effects caused by the future earthquake are observed. For example, the deformations cause strain accumulation in the crust which can be measured by strain gauges and tilt meters (Yoshihisa et al., 2002) as well as by GPS (Kostoglodov,2003), predict formation of cracks within the preparation zone and this will result in changes in seismic wave velocity, density, electric resistivity, ground water level (Khalilov, 2005). All these changes can be monitored experimentally. The ground surface projection of the spherical earthquake projection zone is given by Dobrovolsky *et al.*, 1971 as $\rho = 10^{0.434} M$ km or $\log \rho = 0.434 M$.

- [1] Increase of radon concentration in air.
- [2] Increase of electric field near ground level.
- [3] Increase of ground temperature.
- [4] Decrease of relative humidity of air.

Continuous Monitoring of the above precursors and their real-time recording at a Central Station have been planned at CES. This will be more effective and advantageous than random measurements taken now and then elsewhere so far. Also, for the non-circle target zone, it is better to fit a circle to the range of study area and then finding this value. Afterwards, for each disturbed station (stations which show anomaly), a circle of radius $R = R' + dr$ has been drawn which called 'investigation circles' (In.Cs). After drawing the In.Cs, 'Expectation circle' (Ex.C) is defined as a circle of radius R which its center being within the target zone And finally, the springs which located within the Ex.C are called 'Expectation Springs' and denote by Ex.Ss.

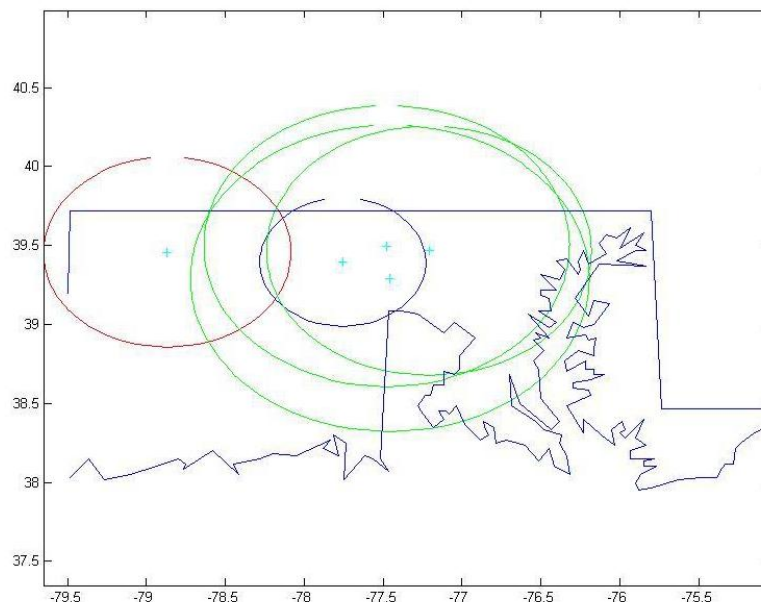


Figure5. Sensing Range Identification based on Inner and Outer Expectation Circles

For Early Warning based on WSNs, the stations (the seismological term) or nodes (networking term), are deployed in the city itself, that is, where the damaging is to be expected. This approach is called an On-site system – in contrast to Front-detection systems, where the stations would be placed near to the hot springs. D/R ratio is described which D is the strain radius and R is distance between monitoring station and earthquake epicenter (km). Radius of the zone within which precursory phenomena may be manifested (so-called strain radius R in Dobrovolsky equation). First of all, the “target zone” has been defined as the study area which constituted from porous cracked saturated rocks and with high capacity of cracks growth during increasing tectonic stress. In this distinctive zone, a radon monitoring measurement in soil and groundwater has been implemented (radon precursory study in soil and groundwater is quite difference in measurement methods, but not in interpretation with seismic events). if any anomaly has been observed in two or more than two monitoring stations, the distance between the farthest of them and the center of target zone (R^*) has been measured. In this study—and by most scientists—an anomaly defined as radon concentration spike crossing $\bar{x} + dr$ where \bar{x} is the average and dr , the standard deviation. Then several kilometers according to vastness of target zone must be added to this measured value as “uncertainly parameter” (dr). Because, Dobrovolsky equation has been defined for a centralized prepare zone; not for a wide area. For example, if the target zone is a circle of radius 5 km and the monitoring station located at the center of this area, the uncertainly parameter is considered 5 km. Also, for the non-circle target zone, it is better to fit a circle to the range of study area and then finding this value. Afterwards, for each disturbed station (stations which show anomaly), a circle of radius $R = R^* + dr$ has been drawn which called ‘investigation circles’ (In.Cs) as shown in Figure 5. After drawing the In.Cs, ‘Expectation circle’ (Ex.C) is defined as a circle of radius R which its center being within the target zone. And finally, the springs which located within the Ex.C are called ‘Expectation Springs’ and denote by Ex.Ss. Proposed algorithm establishes a new high accuracy method to obtain the range of location and magnitude of a coming earthquake for a target zone. In the first step, we assume that between these hot springs, three of them indicate anomaly in radon concentration (for example A1, A2 and A3). In the second step, according to proposed algorithm distance between A3 and center of city X—which introduced as target zone—is about 84.6 km (R_0) which is more than the other distances. So, we nominate the A3 as the farthest station which anomaly has been observed. In third step, by considering the vastness of Xth city, it is inferable that $dr = 10$ km should be added to R_0 . $R = R_0 + dr = 84.6 + 10 = 94.6$ km. In the next step, we draw a circle of radius 94.6 km to the center of Xth city as Ex.C (red circle). Between the all selected hot-springs, four of them located within this circle: A1, A2, A3 and A4. Then we draw four circles of radius R in the center of these hot-springs as In.Cs. The area of interface between these four In.Cs becomes 1,477 km² which illustrate the location of coming earthquake. Also, between the undisturbed hot-springs, Station C is the nearest station to Xth city which lies outside of Ex. C. Therefore, according to Table 2 and considering $dr = 10$ km for X—as described before—we have: $L = L_0 + dr = 109.2 + 10 = 119.2$ km. The capability of proposed algorithm to implementation in all kind of geological structures because Dobrovolsky equation has been examined in different structures whereby capability of proposed algorithm to design various continuous radon monitoring networks in soil and groundwater to predict earthquakes.— Proposed algorithm can be used for all geochemical precursors to predict earthquake. Have some sensing range and complete coverage of detected area D if A_i denotes the size of area covered by i^{th} placed sensor node. Minimum number of working nodes is equivalent of minimum of size of overlap region and can be calculated as shown below.

Our research is based on boolean sensing model where sensor node can detect only events that are within certain range of it for a circular article. Let r denote the sensing range of each node, and l denote the radio range. It has been proved that if the radio range is at least twice the sensing range, complete coverage of a convex area implies connectivity among the working set of nodes. Assuming that n sensor nodes are randomly distributed over radius R region. Set of $\{S_1, S_2, S_3, \dots\}$, for all $1 \leq i \leq n$, let A_i denote the size of area that is covered by the i^{th} placed sensor node, A denote the size of the whole detected region D $A = \pi R^2$. The multi-coverage problem can be described that seek a subset S' , making maximum coverage fraction $R(S')/S$ and minimum number of working sensor nodes S' . Capability of proposed algorithm to design various continuous radon monitoring networks in soil and groundwater to predict earthquakes. Anomalies in radon concentration have been observed in only nine of hot-springs. Proposed algorithm can be used for all geochemical precursors to predict earthquake .using minimum number of nodes for this analysis is a task which all need to

take care of regional coverage, point coverage and barrier coverage. The probability of any node distributed in sub-region D' , $D' \subset D$, is related only with the size of D' , so $p = A_{D'} / A_D$. Therefore, for all $1 \leq i \leq n$, sub-object function of coverage fraction is $f(x) = R(S') = A_{D'} / A_D$ in which D' is the size of the region that is covered by S' . Thus we have $E_{CQ} = [\dots]$. The proportion of the number of working nodes S' , to the total number of nodes S , is the sub-object function of the number of working nodes. $W_1 A_{D'} / A_D + w_2 (1 - S' / S)$. w_1, w_2 are the weights of sub-object function. $p(x, y) \in D$, the neighbor of it definite as follows: $K(x, y) = \{ \forall (x', y') \in D \mid ((x' - x)^2 + (y' - y)^2 \leq r^2) \}$. Let A_i denote the size of area which is covered by i th placed sensor node, and X_i denote the extra coverage area contributed by the i th placed sensor. $E[A_i] = E[A] = 1/A$

Let $G_i = X_i / A_i$ be the proportion of the extra coverage area contributed by the i th placed sensor to its node coverage. We have $E C_1 = E X_1 = E A$ and $C_i = C_{i-1} + X_i$ for all $i, 2 \leq i \leq n$ $E[C_i] = E[C_{i-1}] + E[X_i]$

$$E[X_i] = E[G_i] * E[A_i]$$

As sensor nodes are uniformly distributed, G_i is expected to be the proportion of the uncovered area to the whole deployment area.

$$E[G_i] = A - E[C_{i-1}] / A$$

$$E[C_i] = E[C_{i-1}] + A - E[C_{i-1}] / A * E[A_i]$$

which A_i^j denote the size of j -covered area after i sensor nodes have been placed in j

Y_i^j denote the extra area to the sensor region of i th placed sensor node to the size of j -covered region, P_i^j is the proportion of Y_i^j to A_i . According to (5) and (6), we have

Reducing the overlapping area to reduce the number of working nodes, the lifetime of wireless sensor networks can be prolonged. Since $E[A]/A$ is the probability of link occurrence p , $A = \pi r^2$, and $E[C_n]$ expressed as follows: we can obtain the result to k -coverage problem. For all $0 \leq i \leq n, 0 \leq j \leq k$, and i, j .

$$E[C_n] = [1 - (1 - r^2/R^2)^n] A$$

The equation will help us to analyze network life vs number of nodes with full coverage R and initial amount of energy of each node for considering a cellular pattern of k range

$$0 \leq i \leq n, 0 \leq j \leq k \text{ and } i, j.$$

$$E[A_i^j] = E[A_{i-1}^j] + E[Y_i^j]$$

$$E[Y_i^j] = E[P_i^j] + E[A]$$

Where by A_i^j is size of the j covered area after i sensor nodes has placed ; Y_i^j is extra area to sensor region of i th placed sensor node to the j covered region. P_i^j is proportion of Y_i^j to A_i . $E[P_i^j] = E[Y_i^j] / E[A] = E[A_{i-1}^j] - E[A_{i-1}^j] / A_i, 0 \leq i \leq j$

$$E[A_i^j] = (1-p) E[A_{i-1}^j] + p E[A_{i-1}^{j-1}].$$

Lemma 1: if $S_i \in \{S_1, S_2, \dots, S_n\}$

Have some sensing range and complete coverage of detected area D if A_i denotes the size of area covered by i th placed sensor node. Minimum number of working nodes is equivalent of minimum of size of overlap region for $A = |D|$ size of area covered by i th node for degree of overlapping coverage at any point where $H(x) = \text{If } x \in I_R(x) = 1 \text{ or else } I_R(x) = 0$; And if $x \in I_i(x) = 1 \text{ or else } I_i(x) = 0$; $L = n|A_i| - |D|$. By reducing the overlapping area to reduce the number of working nodes the lifetime of sensor networks can be prolonged. Consider a deployment region of size A . Let a denote the size of nodes sensing region outside the detected area R'' , P denote the probability of n sensor nodes coverage. Given a fixed sensory range such that the expected node coverage is $E[N]$, the number of sensor nodes is suffice for this inequality. As the proportion of the sensing range of nodes to the range of deployment area is known, the number of nodes needed to placed to achieve the multi-coverage fraction can be estimated that achieved the coverage and connectivity requirement.

$$\frac{\log(1-P)}{\log(1-E[N]/A)} < n < \frac{\log(1-P)}{\log(1-E[N]/A+a)}$$

$$\log(1-E[N]/A) \quad \log(1-E[N]/A+a)$$

Size of the sensing is πr^2 ignoring the bordering effects probability of each point $p(x,y) \in D$ covered by at least one node is equal to the probability of the node distributed in the neighborhood.

The probability of one node sensing whole area is $\pi r^2/A$

Probability of two nodes $P_2 = P(A) + P(B) - P(A)$

$$= p + p - (p * p)$$

$$= 2p - p^2$$

Probability of three nodes $P_3 = P_2 + p - P_2 * p$

$$= 2p - p^2 + p - (2p - p^2) * p$$

$$= 1 - (1 - p)^3$$

By mathematical induction we can deduce that $p = 1 - (1 - p)^n$

$$N = \log(1 - p) / (1 - \pi r^2/A) = \log(1 - p) / \log(1 - \pi r^2/A)$$

$$n > \log(1 - P) / \log(1 - \pi r^2/A)$$

This shows that proportion of sensing range to range of deployment area is known the number of nodes needed to be placed to achieve multi-coverage fraction can be estimated that achieved coverage and connectivity requirement.

5. CONCLUSION

The design of the device is a representation of an innovative approach in construction of an earthquake warning and alert system. The system uses two different subsystems and detects the change in the strain pattern by the subsystems. All sensors used are readily available and cheap thus making it a user friendly and affordable product. The Radon monitoring stations should be deployed in quite stable rocks within blocks of the slowest "secular motion" selected from three or four years of GPS data. The LM324 is found to have very poor input and output range especially when working on a single supply and would require two or more Radon detection units. Secondly, the low frequency characteristics can be changed based on the RC time constant in the circuits involved. Proposed algorithm establishes a new high accuracy method to obtain the range of location and magnitude of a coming earthquake for a target zone. Increasing the accuracy of results could be obtained with increasing the number of radon monitoring stations.

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