

Wastewater and Magnetized Wastewater Effects on Soil Erosion in Furrow Irrigation

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Abstract: *In this paper we investigated the effects of fresh water (F as a control), wastewater (W) and magnetized wastewater (M) on furrow erosion. Experimental design was randomized complete blocks consisting of four replication blocks and three water quality treatments. Five irrigation events with 4 days' irrigation interval were practiced in each furrow. The erosion was monitored and measured in the second, fourth and fifth irrigation events for each furrow. Water quality parameters measured during the irrigation ventsd included cations, anions, EC, pH, total-coliform, TSS, DO and COD. The applied intensity of the magnetic field was 10 mili-Tesla. Furrows spacing, length and slope were 0.6 m, 42 m and 0.11 %, respectively. Inflow rate was 0.8 l/s for all the irrigation evens. To determine the net erosion in furrows, water samples were taken from runoff after its start at different time intervals. The net erosion was calculated at each time after determining soil mass in the samples and the net erosion vs. time chart was plotted. The mean erosion was calculated from this chart. The erosion indexes investigated in this study include mean erosion and maximum depth of the furrow cross-section. The results showed that, in all of the water treatments, the net erosion decreases with time in each irrigation., There is also a significant decrease in the mean erosion values in W and M treatments, compared with F treatment, in the second and fourth irrigation events at the 1% ($p < 0.01$) and 5% ($p < 0.05$) level, respectively, but there no significant difference between W and M treatments. The effect of irrigation event on the mean erosion was not significant in any treatment. The effect of water treatment on the basic infiltration rate and the maximum depth of furrow cross-section were not significant, but the basic infiltration rate was in most cases higher in M treatment than in F and W treatments in most cases. Also the changes in the maximum depth of furrow cross-section due to subsequent irrigation events were smaller in M and W treatments than in F treatment.*

Keywords: *Water quality; Wastewater; Magnetic field; Magnetized wastewater; Runoff; Furrow erosion; Net erosion*

1. INTRODUCTION

1.1. Soil Erosion

Erosion due to irrigation has been studied primarily in North America in 1940 (KOLUVEK et al, 1993). Irrigation-induced erosion and subsequent sediment loss is a serious agricultural and environmental problem (CARTER et al, 1993). Soil erosion decreases soil productivity, because, for example, the furrow erosion on irrigated land decreases topsoil depth in the upslope part of the field area and may increase the topsoil depth in the downslope part, reducing thereby the soil productivity potential (CARTER, 1993). Erosion is more common when water moves in small channels called furrows (TROUT and NEIBLING, 1993). Soil erosion due to irrigation, especially furrow irrigation, contributes to the nonpoint-source pollution of water (HAJEK et al., 1990) and is a serious threat to crop productivity in many regions (CARTER, 1993). It may damage water quality in rivers, lakes and streams (BJORNEBERG et al., 2005). A large amount of farm soil may be lost due to furrow erosion

caused by runoff from furrows that transfers sediment (CARTER, 1993). Soil erosion and thus increase of the suspended solids amounts, causes water turbidity increasing and also decreasing of the water storage capacity of small reservoirs for the upstream residents. Turbidity fluctuating by erosion makes water treatment difficult and also results in the decrease of water storage capacity in the dams. When turbidity concentration increases thus using of chlorine increases for water treatment. To avoid these problems should be done integrated land use management to good maintain of surface water quality (STHIANNOPKAO et al, 2007). Erosion reduces soil physical quality indexes such as water holding capacity and soil structural stability (WALLACE and TERRY, 1998).

Three main factors influencing furrow erosion are the shear stress of flowing water on the furrow perimeter, cohesivity of soil particles (which affects the stability and size distribution characteristics of furrow soil), and stream transport capacity (KEMPER et al., 1985; TROUT and NEIBLING, 1993). Hydraulic forces of water movement and soil parameters such as aggregate stability and particle size will determine erosion and sedimentation (CLEMMENS and BJORNEBERG, 2005). FORNSTORM et al (1985) reported that furrow erosion has more dependence to flow rate, slope, soil texture, furrow length and cross-section (FORNSTORM et al., 1985). BROWN et al (1989) found that in more of the furrows, the furrow cross-section creates by erosion at the first test and will not change significantly during the next experiments (BROWN et al., 1989).

1.2. Water Quality Effect on Soil Erosion

Water quality is one of the important factors in furrow erosion that there are few studies about it. Water quality may influence flow shear by controlling furrow intake and, hence, down furrow flow rate (FIREMAN and BODMAN, 1940; QUIRK and SCHOFIELD, 1955; FRENKEL et al., 1978). Water quality affected soil cohesivity by altering clay dispersion (VELASCO-MOLINA et al., 1971; FRENKEL et al., 1978; MALIK et al., 1992; SHAINBERG et al., 1992) and aggregate stability characteristics in furrow irrigation (SMITH et al., 1992).

Water chemistry may influence the sediment transport capacity of the furrow stream indirectly via impacts on flow shear (i. e. infiltration-induced flow rate effects), and by modifying the character of entrained soil particles and aggregates. Water quality affected flocculation, which determined the size and density of detached soil materials (ARORA and COLEMAN, 1979; GOLDBERG and GLAUBIG, 1987).

WISCHMEIER and MANNERING (1969) reported that water acidity increases the amount of erosion (WISCHMEIER and MANNERING, 1969).

Increasing EC of irrigation water enhanced soil flocculation (ARORA and COLEMAN, 1979) and increased settling rates of sediment suspended in water (ROBBINS and BRICKWAY, 1978). LENTZ et al. (1996) determined that main effects for water quality, traffic, and first vs. second irrigations were significant for total soil loss, mean sediment concentration, total outflow, net infiltration and advance time. Average tail-water soil losses was also most for low EC/high SAR of water treatments and net infiltration decreased 14% in high SAR compared with low SAR treatments too. Soil loss increased 68% for second irrigations, and net infiltration fell 23% in trafficked furrows, but water-quality effects were the same (LENTZ et al, 1996).

1.3. Wastewater and its Effect on Soil Properties

Wastewater irrigatin can be useful for decreasing of erosion and desertification, because arable lands continue to be degraded by erosion and desertification and compost made with municipal waste could be used to increase the nutrition and water-holding capacity of the soils at risk of desertification, thereby maintaining productivity and soil stability near the edge of the desert (MADISON et al, 2004). Irrigation is an excellent user for sewage effluent consumption because sewage effluent is mostly water with nutrients. Using wastewater for irrigation is unrestricted provided it has no adverse effects on crops, soils, animals and humans (BOUWER and IDELOVITCH, 1987).

Effects of irrigation with treated wastewater on soil properties were investigated in many researchers. For example, a four-year study observed a significant decrease of pH and infiltration rate, and a significant increase of organic matter (OM), sodium adsorption ratio (SAR) and electrical conductivity (EC) in the soil irrigated with treated wastewater rather than well water or rain-falls.

Significant reduction of the water infiltration rate caused by a seal formation was mainly attributed to the accumulation of suspended solids, and partially to clay dispersion and microbiological activity (BEDBABIS et al, 2014). Wastewater irrigation significantly affected soil K but not soil P and total soil N. Change of irrigation system can be causes different effects when using treated wastewater too: studies show that surface irrigation than subsurface irrigation significantly decreases soil EC, Sodium (Na) and Magnesium (Mg) at depth of 0-15 cm (HEIDARPOUR et al, 2007). About wastewater effect on soil clogging was found that this phenomenon development is highly correlated with the cumulative mass density loadings of total biochemical oxygen demand and suspended solids (SIEGRIST and BOYLE, 1987). This phenomenon results infiltration decreasing.

SEPASKHAH and SHAHABIZAD (2010) found wastewater causes greater irrigation runoff and soil erosion than freshwater. This occurred due to the differences in quality of wastewater and freshwater (SEPASKHAH and SHAHABIZAD, 2010). It is anticipated that application of the wastewater with higher values of EC and SAR dispersed the soil particles and resulted in crust formation on the soil surface (KAZMAN et al, 1983 and MAMEDOV et al, 2000). Runoff and soil loss from the treated wastewater (with less EC) were significantly lower than those from the saline-sodic water (MANDAL et al, 2008).

1.4. Magnetized Water

Application of magnetized water for irrigation is recommended to save irrigation water. Because for example the researches show that the mean soil moisture contents at below the emitter for the magnetized irrigation water are more than the nonmagnetized irrigation water, and the differences are significant, as the irrigation with magnetic water as compared with the non-magnetic water increases highly significant soil moisture up to 7.5% (MOSTAFAZADEH-FARD et al, 2011). According to these results, the use of magnetized water in trickle irrigation reclaim soils with high cations and anions content such as calcium, sodium, and bicarbonate. Studies showed that magnetized irrigation water decreases mean soil cations (such as calcium, sodium, and magnesium) and anions (such as bicarbonate, chloride, and sulfate) in soil below the emitter relative to nonmagnetized irrigation water. This was caused by greater leaching of soil salt by the magnetized irrigation water (MOSTAFAZADEH-FARD et al, 2012). Moreover, the magnetized water increased yield and yield component traits of all crops (HOZAYN et al, 2011).

(OSTAD-ALI-ASKARI et al, 2015 and OSTAD-ALI-ASKARI et al, 2016 and OSTAD-ALI-ASKARI et al, 2017).

Because of the erosion importance and the extensive use of treated wastewater in irrigation, in this paper wastewater effects on soil erosion were investigated in furrow irrigation. Application of magnetic field technology was also investigated in this subject as magnetized wastewater.

(OSTAD-ALI-ASKARI et al, 2015 and OSTAD-ALI-ASKARI et al, 2016 and OSTAD-ALI-ASKARI et al, 2017 and SAYEDIPOUR et al, 2015).

2. MATERIALS AND METHODS

2.1. Experimental

For investigation of wastewater and magnetized wastewater effects on soil erosion in furrow irrigation a farm research was selected in Isfahan University of Technology (Location: N 32^o42' and E051^o32') in year 2013 for 6 months. The climate of this region was hot and dry and measured air temperature at the weather station in field was from 24.9^oC to 40^oC during all of the experiments.

Some of field soil properties are shown in Table 1.

Table 1. Properties of soil (plow layer)

Depth cm	Particle-size distribution			Textural class USDA	Organic materials %	EC _e ds/m	pH _e -	Bulk density gr/cm ³	Initial volumetric moisture %
	Sand %	Silt %	Clay %						
0-15	50.4	21.8	27.8	Sandy clay loam	< 1	0.93-1.94	7.28-8.58	1.45-1.73	4.0
15-40	52.3	20.3	27.4	Sandy clay loam	< 1	0.81-2.49	7.51-8.50	1.56-1.79	4.2

Note: EC_e = Saturation extract electrical conductivity; pH_e = Saturation extract acidity.

As can be seen in Table 1, soil texture is coarse and initial soil moisture is low.

Three water-quality treatments were used consisted of fresh water (F as control treatment), effluent of wastewater (W) taken from an aeration lagoon (Fig1) and magnetized of the same effluent (M).



Fig1. Urban wastewater treatment plant with aeration lagoon method from two sides

To water transfer into the furrow head with constant inflow rate, a set was used consists of tanks of water supply, reservoir under constant head (Fig. 2) and flexible gated pipe. Two tanks were used to water supply with a total volume of 16 cubic meters in upstream end. A concrete stand with height of 60 cm was also built for creating of hydraulic gradient to water transfer from tanks to reservoir and then tanks were put on it. This stand was caused height difference of about 30 cm between tanks outlet and reservoir inlet. Two brass floater valves of 2 inches were also used to fix of water level in the reservoir.



Fig 2. Wastewater and fresh water reservoirs and stabilizer reservoir of water level

Implementation operations of the research were started with tillage. At this stage, plowing operations, disking and roller-harrowing were done on the field. Then regular gridding was done by surveying and then field was leveled. In next step non-wheel traffic furrows with spacing 0.6m, slop 0.11% and 42m length were made via furrower set. After tillage and furrow making, field slope was determined and then using conditions of maximum recommended non-erosive stream size (given by $Q = 0.6/s$ where Q is the furrow inflow rate, l/sec, and s is the furrow slope in percent) and a constant flow rate taken from the water reservoir, the inflow rate was determined 0.8 l/sec in each furrow.

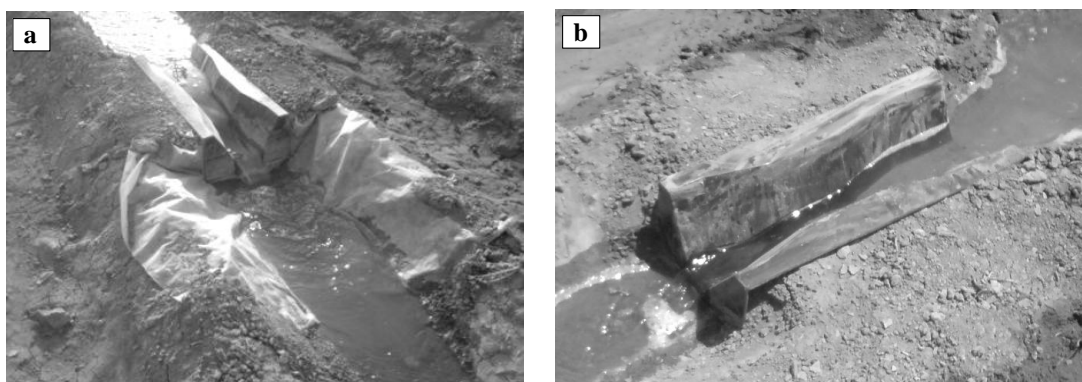


Fig3. Inflow rate measurement (3a); Outflow rate measurement; and sampling of runoff from here (3b)

Gated pipe was attached to the reservoir outlet and using a graduated container and a timer, opening amounts of the valves on the gated pipe were marked for exact creating of the requirement inflow rate

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(0.8 l/sec) and then were opened for specified amount in each experiment. Experiments of related to F treatment were done firstly then for W and M treatments (i. e. gated pipe was used just for F treatment in 20 first irrigation events then for W and M treatments in 40 next tests).

Inflow and outflow rate were measured with WSC¹ flumes of type 2 (Fig3a, b) and their hydrographs were plotted. Basic infiltration rate (f_o) was calculated from the difference between fixed inflow and outflow rate and dividing this difference by the length of the furrow

Five irrigations were applied to in each furrow every 4 days. Soils were with no planting. The erosion was monitored and measured in the second, fourth and fifth irrigation events for each furrow.

The magnetic set was consisting of three magnets each with a 10mT intensity of the magnetic field. Magnets were closed around of the gated pipe with angle of 120 degrees (Fig4).

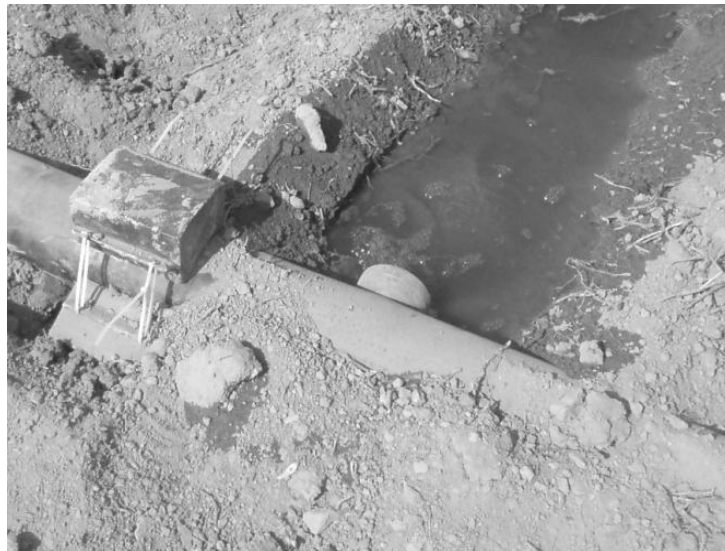


Fig4. *Magnetic set; magnetized wastewater; and gated pipe*

Inflow water-quality parameters were measured at three times before the second, fourth and fifth irrigation events. These parameters were consists of cations (Na^+ , K^+ , Ca^{2+} and Mg^{2+}), anions (HCO_3^- , CO_3^{2-} , SO_4^{2-} and Cl^-), EC, pH, total-coliforms¹, TSS, DO and COD. Total-coliform and COD were measured via multiple-tube fermentation and closed reflux spectrophotometric tests respectively. Fresh water quality was almost constant in all experiments. Water quality experiments were done based on standard methods for the examination of water and wastewater (ANONYMOUS, 1998).



Fig 5. *Main and lateral furrows; water advance to end*

The net erosion (sediment lost in runoff) was determined for each furrow using of KOLUVEK et al (1993) method. After starting of runoff (after water advance to the furrow end (Fig. 5)), samples were taken from it (Fig. 3b) at different time intervals.

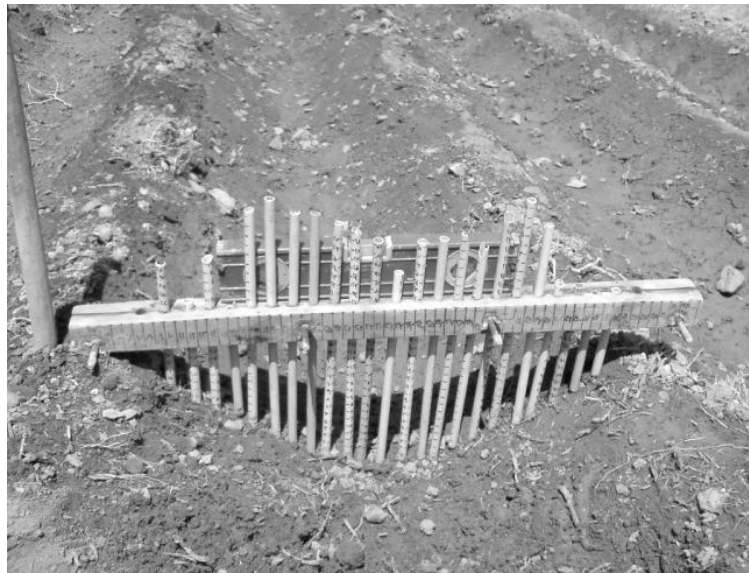


Fig6. Profile Meter Set

Samples volume was the same at each time. 4 or 5 samples were taken during each irrigation event from start to end time of the runoff at specific time intervals (nearly every 5 minutes). The runoff samples were dried in oven at 105°C for 24 hours to measure soil mass value. Then sediment mass determined by difference of wet and dry mass.

(OSTAD-ALI-ASKARI et al, 2015 and OSTAD-ALI-ASKARI et al, 2016 and OSTAD-ALI-ASKARI et al, 2017 and SHAYANNEJAD et al, 2015 and).

The sediment core was calculated from soil mass value divided by water volume for each sample. Then sediment core curve was plotted as a function of time for each irrigation. The mean sediment core at runoff time was calculated from this curve that is area under the net erosion curve divided by runoff time. The total of the net erosion was calculated from multiplication the total volume of runoff by mean sediment core. The total of erosion is total of displaced soil along the furrow that moves to the end.

(RAEISI-VANANI et al, 2015 and SOLTANI-TODESHKI et al, 2015 and ESKANDARI et al, 2017 and RAEISI VANANI et al, 2017)

To study of erosion effect on the furrow shape, cross-section coordinates was measured via profile meter set (Fig6) and maximum depth (Y_{max}) was determined before and after irrigation.

(ESLAMIAN et al, 2017 and GODARZI et al, 2016).

2.2. Statistical Analysis

The experimental design was randomized complete blocks consisted of four replicated blocks with the three water-quality treatments.

Three furrows (one main furrow and two lateral furrows in order to creation of farm actual conditions (Fig 5)) were applied in each plot. Measurements were done in middle furrow.

In this paper statistical analysis was performed on the mean sediment core, f_o and Y_{max} parameters.

3. RESULTS AND DISCUSSION

3.1. Inflow Water and Wastewater Quality

The results of the inflow water and wastewater quality are presented in Table 2. According to this table, the biological parameters and TSS of M and W treatments are different with those of F treatment. So TSS of M and W treatments are 5 times of the other treatment. Magnetic field effects on cations, anions, EC, pH, Total-coliform, TSS and COD of wastewater were investigated. It was found that magnetic field effect on cations and anions does not follow any specific trend, but EC increase slightly. Also was found that magnetic field often increases in pH, TSS, COD and total-coliform in the wastewater.

Table 2. Inflow water and wastewater quality in three irrigation events

Parameters	Unit	Fresh water	Wastewater			Magnetized wastewater		
			Second	Fourth	Fifth	Second	Fourth	Fifth
Na ⁺	mmol/l	5.20	9.50	-	4.80	10.50	-	4.80
K ⁺	mmol/l	0.06	0.90	-	0.30	0.90	-	0.30
Ca ²⁺	mmol/l	2.30	2.25	-	3.10	2.35	-	3.20
Mg ²⁺	mmol/l	0.70	0.85	-	2.50	0.45	-	3.10
HCO ₃ ⁻	mmol/l	7.75	4.40	-	4.90	4.80	-	4.80
CO ₃ ²⁻	mmol/l	0.00	0.00	-	0.25	0.00	-	0.30
SO ₄ ²⁻	mmol/l	0.55	0.79	-	0.15	0.79	-	2.10
Cl ⁻	mmol/l	6.25	10.63	-	10.60	10.63	-	8.10
SAR	(mmol) ^{0.5} /l ^{0.5}	4.25	7.63	-	2.87	8.87	-	2.70
pH	-	7.55	8.26	7.26	8.01	8.30	7.56	7.79
EC	dS/m	0.656	0.990	1.095	1.099	1.002	1.108	1.100
TSS	mg/l	10	60	68	53	61	65	56
DO	mg/l	6.8	-	-	-	-	-	-
COD	mg/l	0	92	110	84	95	102	93
Total-coliform	MPN/100cc	0	23.3 ×104	6.9 ×104	17.6 ×104	35.6 ×104	10.5 ×104	2.0 ×104

Note: SAR = Na/[(Ca + Mg)/2]^{0.5}; MPN: Most Probable Number

3.2. Soil Erosion Analysis

A sample of inflow and outflow hydrographs and net erosion charts are shown in Fig 7.

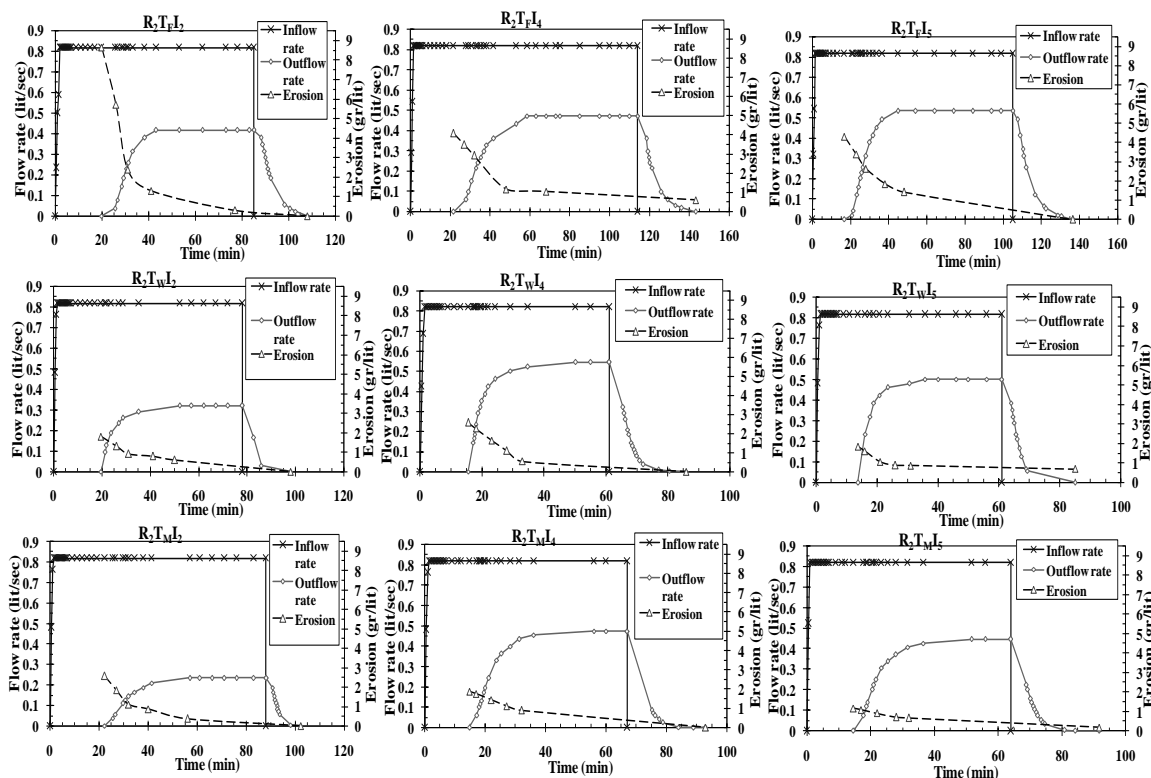


Fig 7. Inlet and outlet hydrographs and net erosion charts for second replication

Note: For example R₂T_fI₂ = Riplication 2, fresh water treatment and irrigation event 2;

R₂T_wI₂ = Riplication 2, wastewater treatment and irrigation event 2;

R₂T_mI₂ = Riplication 2, magnetized wastewater treatment and irrigation event 2.

Results in Fig 7 show that in all of the water treatments net erosion decreases related to time for each irrigation. Mean and total of net erosion were also calculated that are presented in Table 3.

Table 3. Results of mean and total erosion, basic infiltration rate (f_0) and maximum depth of furrow cross-section in upstream end (Y_{max}) and their statistical analysis

Replication	Water treatment	Mean erosion (gr/l)			Total of erosion (gr)			f_0 (mm/hr)			Y_{max} (cm)		
		Irrigation number			Irrigation number			Irrigation number			Irrigation number		
		2	4	5	2	4	5	2	4	5	2	4	5
I	F	0.84	1.98	1.28	718.3	770.7	626.7	85.5	68.2	68.5	17.8	19.7	20.7
	W	0.65	1.11	0.51	1046.6	1854.5	970.3	55.1	47.2	32.1	16.2	17.1	17.6
	M	0.76	0.53	0.56	1923.7	1129.5	1328.1	32.7	25.1	21.5	17.5	18.3	18.8
II	F	1.32	1.27	1.18	1117.4	1843.2	2106.3	57.4	49.5	40.5	16.2	17.8	18.6
	W	0.57	0.59	0.88	636.8	741.6	1289.7	71.1	39.3	45.2	15.1	15.5	15.6
	M	0.55	0.65	0.53	520.2	967.8	745.2	83.6	49.2	53.4	18.9	19.0	19.0
III	F	0.40	0.35	0.43	959.9	724.1	935.5	65.7	50.0	47.0	17.8	19.7	20.7
	W	0.56	0.53	0.45	918.8	860.3	553.7	55.0	51.5	52.2	16.5	17.2	17.5
	M	0.85	0.48	0.37	857.7	715.0	311.9	77.5	52.5	67.3	16.2	17.2	17.7
IV	F	1.04	0.73	1.31	2217.9	1684.6	3030.8	58.0	46.3	55.1	18.8	20.8	21.8
	W	0.82	0.50	0.30	1259.3	1288.9	430.8	47.0	30.1	53.9	15.9	17.0	17.5
	M	0.42	0.51	0.31	1018.2	935.8	597.1	55.0	39.1	42.8	16.5	17.5	18.0
Statistical analysis													
	df												
Water treatment	2	**	*	**	-	-	-	NS	NS	NS	NS	NS	NS
Replication	3	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS	NS
Error	6												
Total	12												
Corrected Total	11												

Note: df = degree of freedom; NS = non significant; * $P < 0.05$, ** $P < 0.01$.

Values of basic infiltration rate, maximum depth of furrow cross-section and their statistical analysis are shown in each irrigation event at Table 3 too. Data in Table 3 show that the mean erosion in W and M treatments has significantly decreased related to F treatment. So, there is a significant difference at 1% level between mean erosion in W and F treatments and M and F treatments for second and fifth irrigation events and 5% for fourth irrigation event (due to water quality, EC, SAR, ..), but there is no significant difference between M and W treatments in all irrigations. The results showed that effect of irrigation events on the mean erosion in all of the treatments was not significant. According to Tables 2 and 3 with increasing amount of suspended and dissolved solids (i. e. capacity reduction of transport soil particles and aggregates) outlet net erosion decreases at the end of the furrows. The results show that increasing in f_0 causes decreasing in net erosion, but it had no significant effect on erosion (Table 3). Increasing in f_0 can be due to high EC in M treatment that is compliant with OSTER and SCHROER, (1979) report. Magnetizing (according to BOGATIN (1999) results) and high EC are causes of f_0 increasing for M treatment than W one. Using M treatment increases soil basic infiltration rate in more cases and this is consistent with findings of BOGATIN (1999). So magnetic field may be cause decrease in net erosion (Table 3) because according to researches of AINA (1993) can be reduced runoff and erosion through improved infiltration capacity.

(OSTAD-ALI-ASKARI et al, 2015 and OSTAD-ALI-ASKARI et al, 2016 and OSTAD-ALI-ASKARI et al, 2017 and SHOJAEI et al, 2017 and BAHMANPOUR et al, 2017)

Soil erosion decreased during irrigation events in W and M treatments (according to Fig 8). We guess that this is due to soil particles stability that can be had a good agreement with results of BISWAS et al (2009). They showed application of effluent increases the soil aggregate stability. Also replacing saline-sodic irrigation water with treated wastewater could have favorable effects on soil structural stability (MANDAL et al, 2008). It is important to note that soil particles stability increases water resistance and consequently decreases soil erosion.

(OSTAD-ALI-ASKARI et al, 2015 and OSTAD-ALI-ASKARI et al, 2016 and OSTAD-ALI-ASKARI et al, 2017).

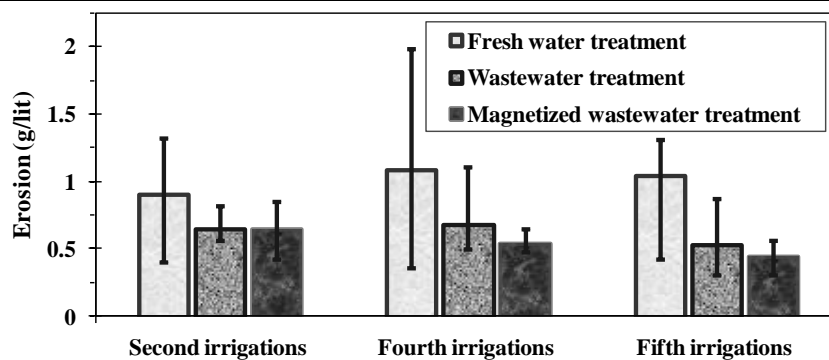


Fig 8. Average erosion in different irrigation events and replications

Note: Error bars show maximum and minimum of the net erosion.

Three water quality treatments caused change in maximum depth (Y_{max}) of the furrow cross-section (Fig. 9 and Table 3).

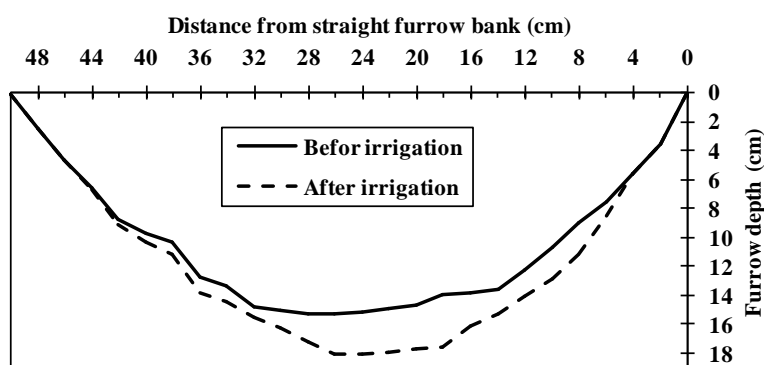


Fig. 9. The sample of furrow cross-section before and after irrigation

Changes of Y_{max} were also calculated in each treatment related to second irrigation event ($(Y_{max_i} - Y_{max_2}) / Y_{max_2}$) that Y_{max_2} is maximum depth in second irrigation event and $i = 4$ or 5) (Fig 10).

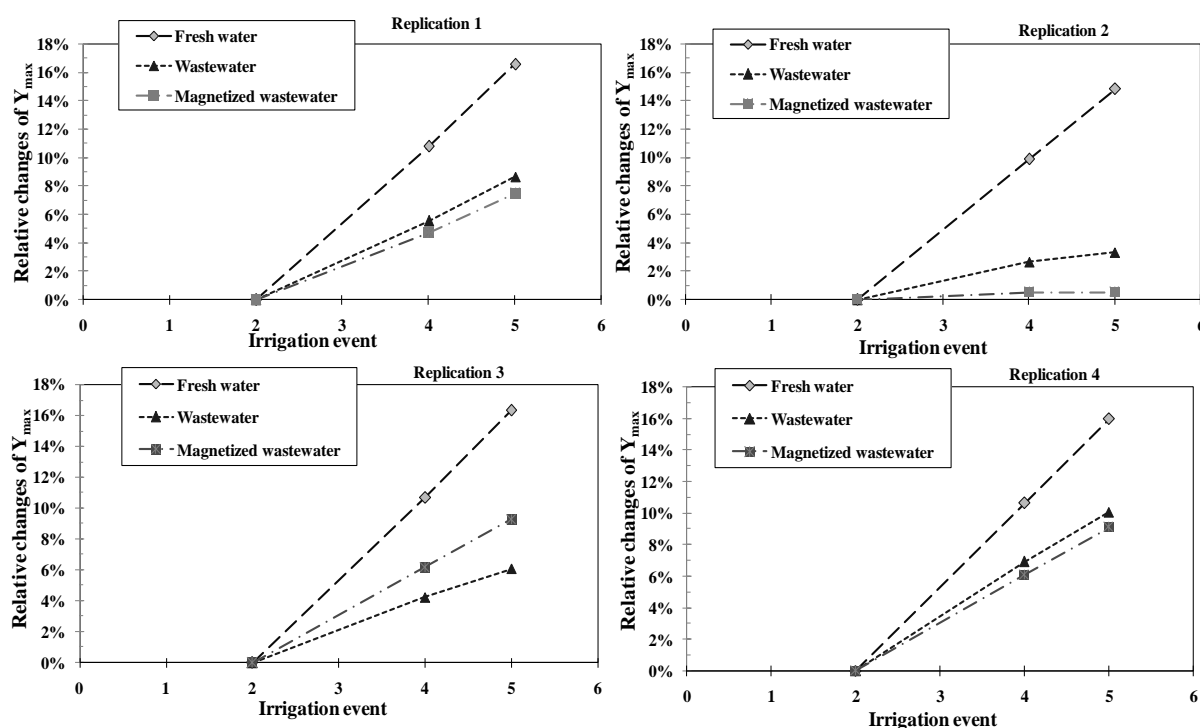


Fig 10. Changes of Y_{max} in different irrigation events than the second irrigation for treatments

According to Fig 10 changes of Y_{max} for F treatment are more than W and M treatments in different

irrigation events that is due to more erosion for F treatment, but there is no significant difference between treatments.

4. CONCLUSION

1. Magnetic field increased EC and pH of the wastewater; also it increased TSS, COD and total-coliform in some cases.
2. In all of the water treatments, net erosion decreases related to time for all of irrigation events.
3. W and M treatments decreased mean erosion significantly relative to F ones. This difference was in the second and fourth irrigation events at the 1% ($p < 0.01$) and 5% ($p < 0.05$) level respectively, but there was no between of W and M treatments. These results confirmed this topic that capacity reduction of transport soil particles and aggregates in water treatments decreases soil erosion by these treatments.
4. Magnetizing of wastewater was caused erosion decreasing for M treatment than W treatment, because magnetizing caused infiltration increasing so that runoff and thereby soil erosion decreased.
5. Basic infiltration rate of the M treatment became more than W and F ones in more cases that can be caused erosion reduction and this results were also true for W treatment than F ones.
6. Changes of maximum depth of furrow cross-section in upstream end for F treatment were more than W and M treatments that shows more erosion for F treatment.
7. Results of erosion investigation confirmed what is already known that are decreasing of the soil erosion and infiltration increasing for high EC in water treatments.
8. According to this paper results, suggest new research for investigation of different intensity of the magnetic field (created by both of constant magnetic field or electromagnetic field) effects on water and wastewater quality and also on soil erosion.

ACKNOWLEDGEMENT

The costs of this research were fully provided by the grant of the Isfahan University of Technology, Department of Water Engineering. The writers sincerely appreciate the technical and friendly assistances from Mohammad Arab, Sayyed Adel Sadeghi, Behnaz Khosravi, Hosein Sheybani, Sajjad Rezaee, Amir Hosein Delfruzi, Arabzadegan, Behnaz Harandizade, Paya Tejarat Company and water engineering, soil science and civil engineering departments, Isfahan University of Technology.

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Citation: H. Raeisi Vanani, et al." Wastewater and Magnetized Wastewater Effects on Soil Erosion in Furrow Irrigation", *International Journal of Research Studies in Agricultural Sciences (IJRSAS)*, vol. 3, no. 8, p. 14, 2017, <http://dx.doi.org/10.20431/2454-6224.0308001>.

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